dynamic processes in cells (*a systems approach to biology*)

jeremy gunawardena department of systems biology harvard medical school

> lecture 4 17 september 2015

recap

$$a_n \frac{d^n x}{dt^n} + a_{n-1} \frac{d^{n-1} x}{dt^{n-1}} + \dots + a_1 \frac{dx}{dt} + a_0 = 0$$

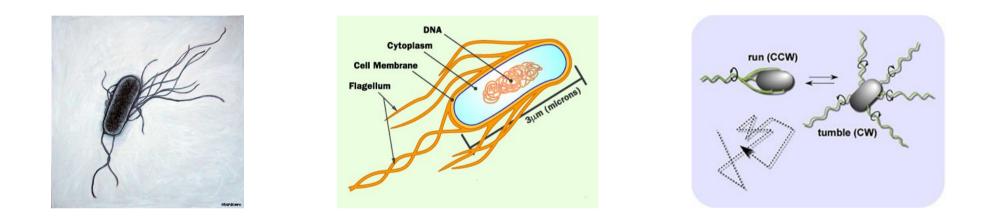
the Laplace transform converts differentiation by s (or t) into multiplication by t (or s)

the solutions of a linear ODE are linear combinations of terms of the form $t^j e^{z_i t}$ where z_i are the roots of the characteristic equation

stable if, for all roots z_i , $\operatorname{Re}(z_i) < 0$

different kinds of negative feedback have different effects - redundancy can be more apparent than real

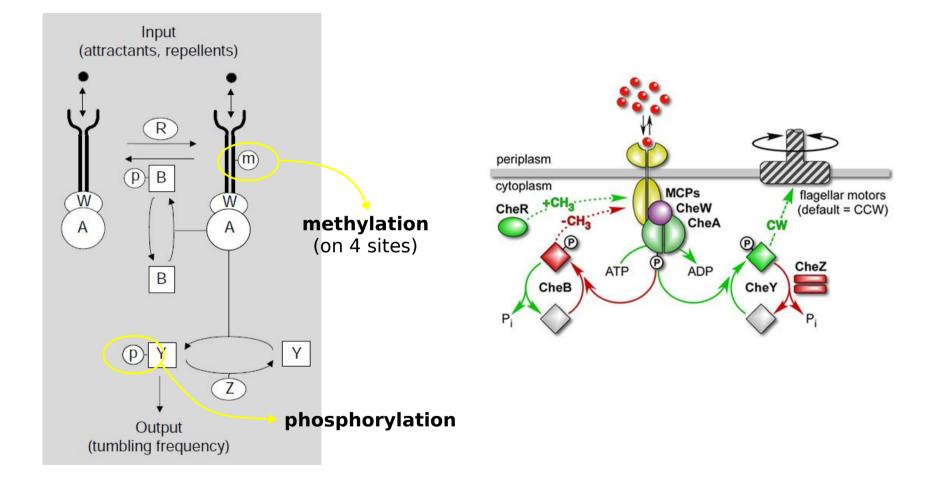
E coli chemotaxis



E coli navigates towards an attractant, or away from a repellent, by rotating its flagella, alternating between **"runs"** (flagella rotating together) and **"tumbles"** (flagella rotating apart). By changing the tumbling frequency, a bacterium can navigate along a chemotactic gradient.

H Berg, E coli in Motion, Springer 2003

molecular circuitry of E coli chemotaxis

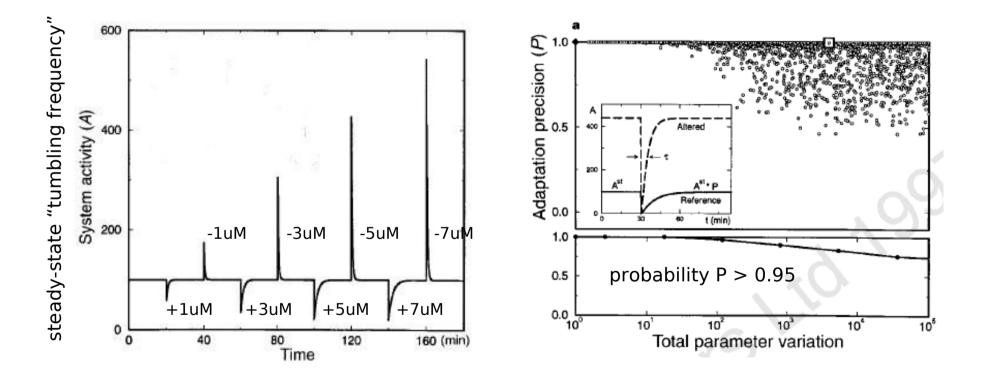


N Barkai, S Leibler, "Robustness in simple biochemical networks", Nature 387:913-7 1997

right hand image here and on the previous slide from Sandy Parkinson's lab @University of Utah - chemotaxis.biology.utah.edu/Parkinson_Lab/

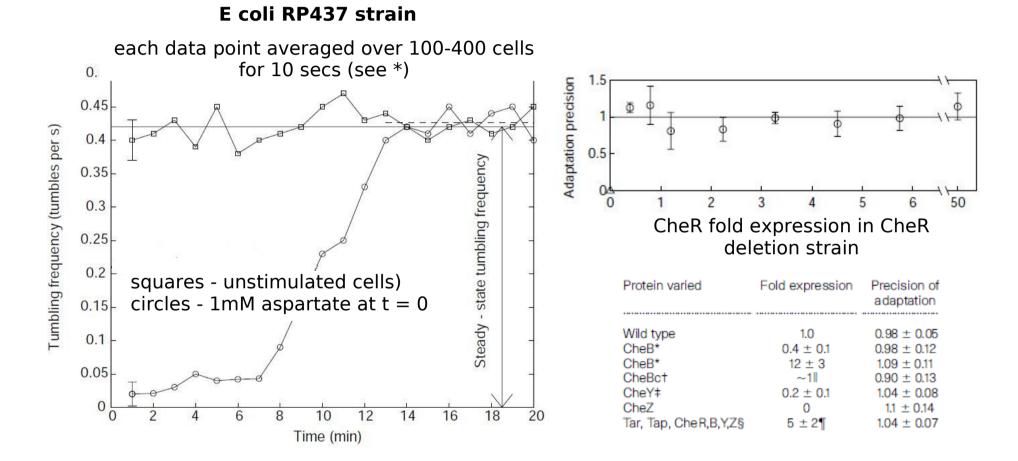
perfect adaptation, in theory

steady-state tumbling frequency returns to its set point after a disturbance, with no steady-state error.



"Figure 3a illustrates the most striking result of the model ... Typically, one can change simultaneously each of the rate constants several fold and still obtain, on average, only a few per cent deviation from perfect adaptation"

perfect adaptation, in practice

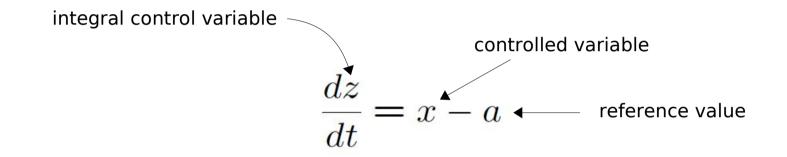


U Alon, M G Surette, N Barkai, S Leibler, "Robustness in bacterial chemotaxis", Nature **397**:168-71 1999

* Korobkova, Emonet, Vilar, Shimizu, Cluzel, *"From molecular noise to behavioural variability in a single bacterium"*, Nature **428**:574-8 2004

perfect adaptation arises from integral control

the Barkai-Leibler model implements integral control, in the sense that a generalised variable, z, can be identified for which



z is approximately the total receptor methylation level in the Barkai-Leibler model



T-M Yi, Y Huang, M I Simon, J Doyle, "Robust perfect adaptation in bacterial chemotaxis through integral feedback control", PNAS **97**:4649-53 2000

matrix formulation

1 component, order n

$$a_n \frac{d^n x}{dt^n} + a_{n-1} \frac{d^{n-1} x}{dt^{n-1}} + \dots + a_1 \frac{dx}{dt} + a_0 = 0$$



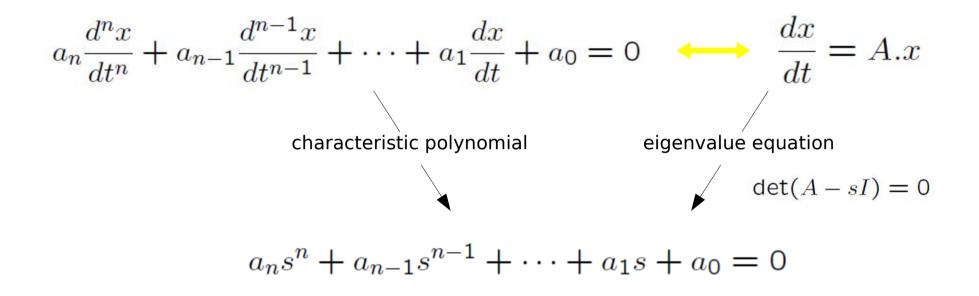
$$\frac{dx}{dt} = A.x \qquad x = (x_1, \cdots, x_n)^t$$

$$x_1 = x, \quad x_2 = \frac{dx}{dt}$$

$$a_2 \frac{d^2x}{dt^2} + a_1 \frac{dx}{dt} + a_0 x = 0 \qquad \qquad \frac{d}{dt} \begin{pmatrix} x_1 \\ x_2 \end{pmatrix} = \begin{pmatrix} 0 & 1 \\ -\frac{a_0}{a_2} & -\frac{a_1}{a_2} \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \end{pmatrix}$$
put matrix in triangular form by
Gaussian elimination

see "Matrix algebra for beginners, Parts I, II & III"

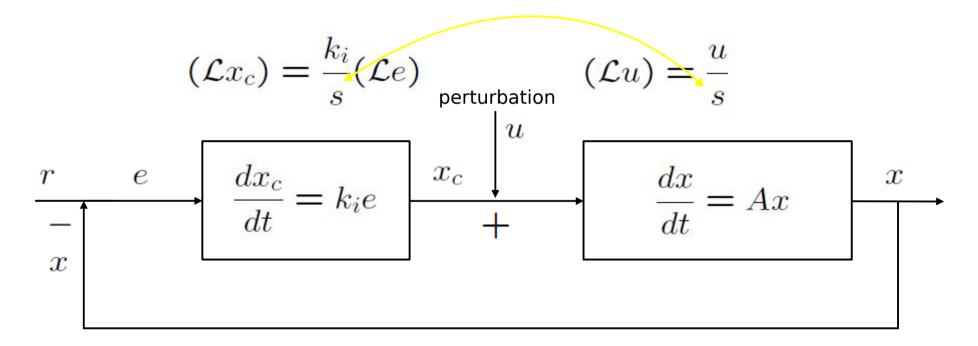
characteristic roots = eigenvalues



in the matrix formulation, the stability condition is that all the eigenvalues of the matrix A have negative real parts

the internal models principle

a controller which perfectly adapts to an additive perturbation must contain an **internal model** of the perturbation

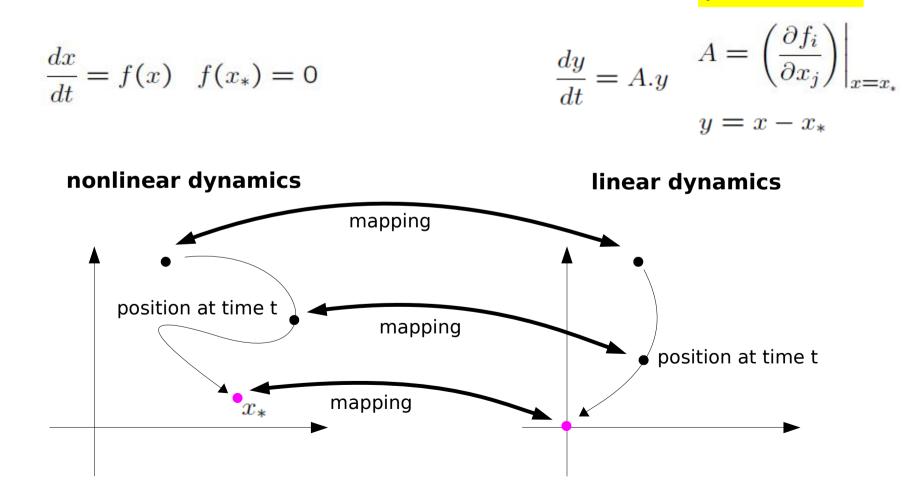


Francis, Wonham, "The internal model principle of control theory", Automatica 12:457-465 1976; E Sontag, "Adaptation and regulation with signal detection implies internal model", Systems & Control Letters, **50**:119-26 2003; M Kawato, "Internal models for motor control and trajectory planning", Curr Opin Neurobiol **9**:718-27 1999.

linear systems approximate nonlinear systems

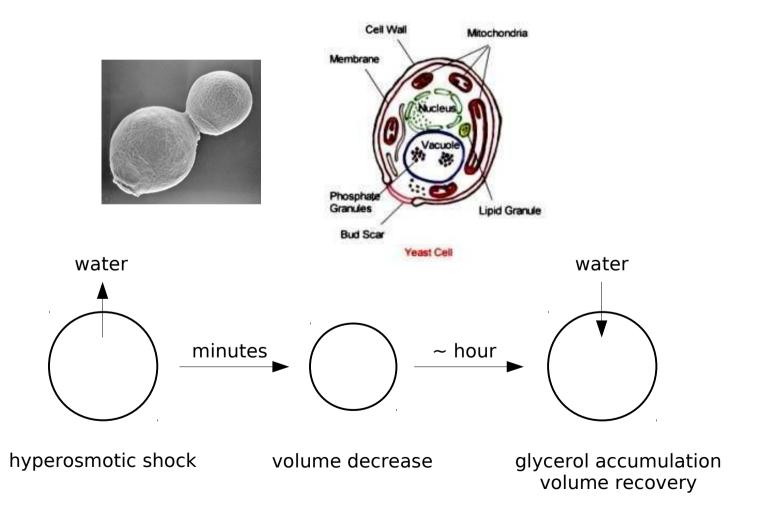
HARTMAN-GROBMAN THEOREM – in the vicinity of a hyperbolic steady state (all eigenvalues of the Jacobian have non-zero real part), a nonlinear system can be qualitatively approximated by a linear one

Jacobian matrix

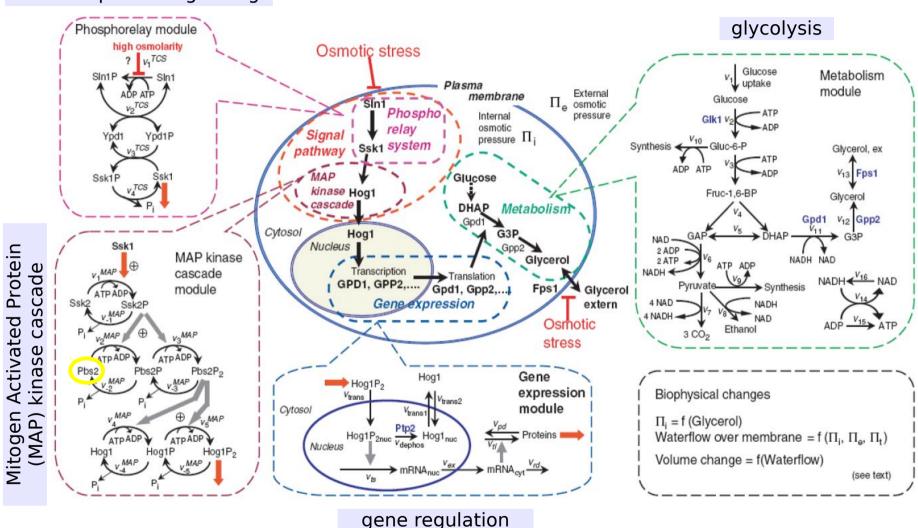


osmolarity regulation in S cerevisiae

yeast are unicellular fungi whose external environment can exhibit changes in osmolarity on fast and slow time scales



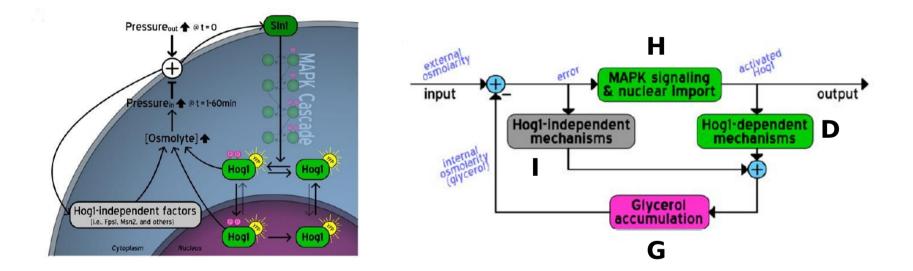
detailed model of the molecular network



two-component signalling

Klipp, Nordlander, Kruger, Gennemark, Hohmann, "Integrative model of the response of yeast to osmotic shock", Nature Biotech 23:975-82 2005

osmolarity regulation as a control system



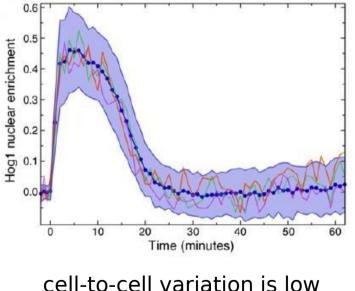
D Muzzey, C Gomez-Uribe, J T Mettetal, A van Oudenaarden, "A systems-level analysis of perfect adaptation in yeast osmoregulation", Cell **138**:160-71 2009

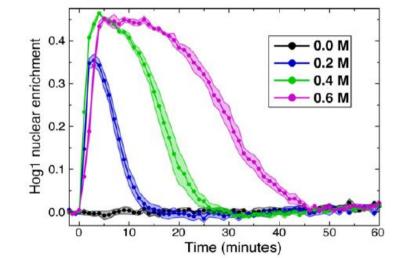
Hog1 nuclear enrichment shows perfect adaptation

Hog1-YFP, haploid SHO1-cells

SHO1 deletion disables the non-Sln1 pathway of Hog1 activation

homeostatic response to step-function increase in external NaCl





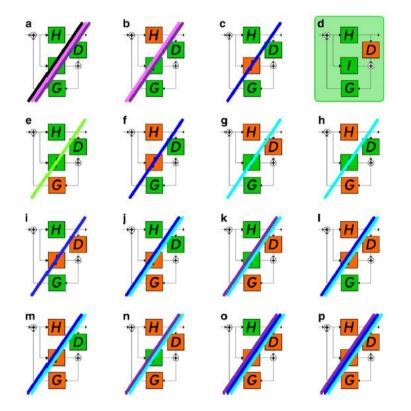
population average returns to its set point perfect adaptation - no steady-state error

perfect adaptation implies integral control in the linear approximation

locating the integral feedback

there is a single integrator, localised to the Hog1-dependent module D

integral control requires Hog1 kinase (Pbs2) activity

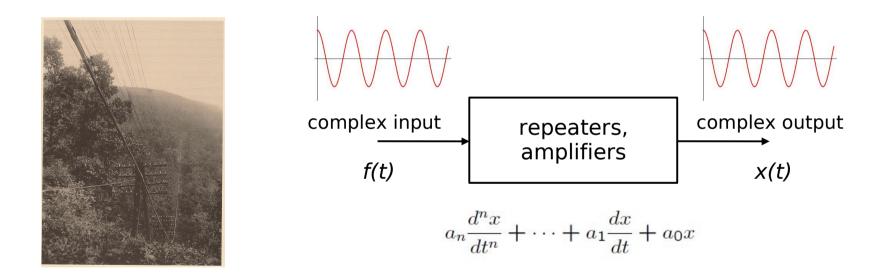


further analysis and extension to Candida albicans:

You, ..., Brown, "A systems biology analysis of long and short-term memories of osmotic stress adaptation in fungi", BMC Res Notes **5**:258 2012

a more complex control problem

trans-continental telephony, early 20th century,



need to ensure that the output recapitulates the input with "high fidelity"

need to understand the input/output behaviour of a highly complex system without knowing all the internal details

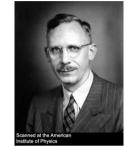
follow the sines

force the system with a sinusoidal input and look at the output

$$f(t) = e^{i\omega t}$$
 $(\mathcal{L}f)(s) = \frac{1}{s - i\omega}$



Hendrik Bode



1889-1976 190

1905-1982

$$a_n \frac{d^n x}{dt^n} + a_{n-1} \frac{d^{n-1} x}{dt^{n-1}} + \dots + a_1 \frac{dx}{dt} + a_0 x = f(t)$$

$$(\mathcal{L}x)(s) = \frac{(\mathcal{L}f) + c(s)}{Z(s)} = \frac{1}{(s - i\omega)Z(s)} + \frac{c(s)}{Z(s)}$$

Hendrik Bode, **Network Analysis and Feedback Amplifier Design**, Van Nostrand, New York 1945

stable system has output at same frequency

if the system is stable, so that the roots of Z(s) have negative real parts, then $i\omega$ cannot be a repeated root

$$(\mathcal{L}x)(s) = \frac{1}{(s-i\omega)Z(s)} + \frac{c(s)}{Z(s)}$$

$$= \frac{B}{s-i\omega} + \sum_{i=1}^{k} \left(\sum_{u=1}^{r_i} \frac{C_{i,u}}{(s-z_i)^u} \right) + \sum_{i=1}^{k} \left(\sum_{u=1}^{r_i} \frac{D_{i,u}}{(s-z_i)^u} \right)$$

$$x(t) = Be^{i\omega t} + \sum_{i=1}^{k} C'_i t^{r_i} e^{z_i t} + \sum_{i=1}^{k} D'_i t^{r_i} e^{z_i t}$$

$$\to 0, \text{ as } t \to \infty \qquad \text{because of stability}$$

after the transients have died down, the response of a stable linear system to sinusoidal forcing is a sinusoidal output at the same frequency

the transfer function

but what is the amplitude, B?

$$\left(a_n \frac{d^n}{dt^n} + a_{n-1} \frac{d^{n-1}}{dt^{n-1}} + \dots + a_1 \frac{d}{dt} + a_0\right) \left(Be^{i\omega t}\right) = Ae^{i\omega t}$$

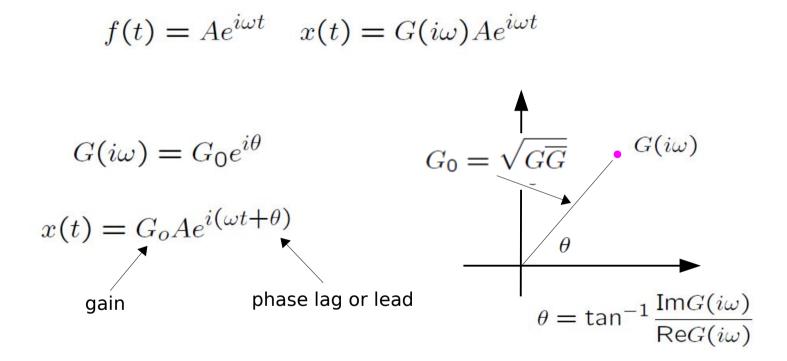
$$B(a_n(i\omega)^n + a_{n-1}(i\omega)^{n-1} + \dots + a_1(i\omega) + a_0) = A$$

$$B = \left(\frac{1}{Z(i\omega)}\right)A = G(i\omega)A$$

the transfer function is the reciprocal of the characteristic polynomial

linear frequency analysis

the amplitude is the transfer function, evaluated at the forcing frequency



for high fidelity, the gain and the phase lag/lead should change little with frequency

second-order linear ODEs

consider a system normalised the way physicists prefer

positive coefficent of x is +1 $\begin{pmatrix} 1 \\ \frac{1}{\omega_f^2} \end{pmatrix} \frac{d^2x}{dt^2} + \left(\frac{2\delta}{\omega_f}\right) \frac{dx}{dt} + x = 0$ $\omega_f > 0 \quad \text{fundamental frequency} \quad (\text{time})^{-1}$ $\delta \quad \text{damping ratio} \quad \text{dimensionless}$

with these choices the characteristic polynomial has the following two roots

$$s = \omega_f(-\delta \pm \sqrt{\delta^2 - 1})$$

and the system is stable provided that $\delta > 0$

